Structures For Discrete-Time Systems

- Realization (implementation) of digital filters
- Structures of IIR and FIR filters, their advantages and disadvantages efficiency and error

Example: Given
$$H(z) = \frac{b_0 + b_1 z^{-1}}{1 - a z^{-1}}$$
 $|z| > |a|$

$$\Rightarrow h[n] = b_0 a^n u[n] + b_1 a^{n-1} u[n-1] \qquad \text{IIR}$$

It is not possible to implement the system by discrete convolution!

$$\Rightarrow y[n] = ay[n-1] + b_0 x[n] + b_1 x[n-1]$$

Actually, an unlimited variety of computational structures result in the same relation between y[n] and x[n]!

When the numerical precision is limited

 \Rightarrow different structures may have vastly different behavior.

- (i) Finite-precision representation of the system coefficients
- (ii) Truncation or rounding of intermediate computations.

♦ Block Diagram and Signal Flow Graph

• Three elements in LTI discrete-time systems:

	Block diagram	Signal flow graph	
Adder	$x_1 \longrightarrow y$ $x_2 \longrightarrow y$	$x_1 \circ \xrightarrow{x_2} \circ x_$	
Scalar (Multiplication by a constant)	x a y	x a y 0 \rightarrow 0	
Unit delay	$x[n] \xrightarrow{7^{-1}} x[n-1]$	$x[n] \xrightarrow{7^{-1}} x[n-1]$	

Nodes and *branches* are keys in a signal flow graph
 Source node: No entering branches
 Sink node: Only entering branches

♦ Basic Structures for IIR Systems

• Direct Forms (1) Direct Form I

$$H(z) = \frac{\sum_{k=0}^{M} b_k z^{-k}}{1 - \sum_{k=1}^{N} a_k z^{-k}} \Leftrightarrow y[n] - \sum_{k=1}^{N} a_k y[n-k] = \sum_{k=0}^{M} b_k x[n-k]$$

$$H(z) = H_2(z)H_1(z) = \frac{Y(z)}{X(z)} = H_2(z)V(z)\frac{H_1(z)}{V(z)}$$

$$Y(z) = H_2(z)V(z) \leftrightarrow y[n] - \sum a_k y(n-k) = v[n]$$

$$X(z) = V(z)/H_1(z)$$

$$V(z) = H_1(z)X(z) \leftrightarrow v[n] = \sum b_k x[n-k]$$

$$V(z) = \sum b_k X(k)z^{-k}$$

$$Y(z) - \sum a_k Y(z)z^{-k} = V(z)$$

$$Y(z) = V(z) + \sum a_k Y(z)z^{-k}$$



Figure 6.3 Block diagram representation for a general *N*th-order difference equation.



Figure 6.14 Signal flow graph of direct form I structure for an Nth-order system.

(2) Direct Form II (Canonic form)

- -- Interchange 1st and 2nd "segments" and merge the delay lines (z^{-1})
- -- Number of delay = $max(N,M) \leftarrow$ "Canonic"



 a_N

 b_N

Figure 6.15 Signal flow graph of direct form II structure for an *N*th-order system.

Cascade Form

-- Serial connection of 1st order and 2nd order factors

$$H(z) = \prod_{k=1}^{N_x} \frac{b_{ok} + b_{1k} z^{-1} + b_{2k} z^{-2}}{1 - a_{1k} z^{-1} - a_{2k} z^{-2}}$$

Remark: Each factor is a Direct Form II.



Figure 6.18 Cascade structure for a sixth-order system with a direct form II realization of each second-order subsystem.

If there are N_S second-order sections

 $\Rightarrow (N_{S}!)^{2}$ different pairings and orderings!

- $\prod_{k=1}^{N_x} \frac{b_{ok} + b_{1k} z^{-1} + b_{2k} z^{-2}}{1 a_{1k} z^{-1} a_{2k} z^{-2}}$ needs 5 constant multipliers for each section.
- $b_0 \prod_{k=1}^{N_x} \frac{1 + \tilde{b}_{1k} z^{-1} + \tilde{b}_{2k} z^{-2}}{1 a_{1k} z^{-1} a_{2k} z^{-2}}$ needs 4 constant multipliers for each section.

The 5-multiplier sections are commonly used when implemented with fix-point arithmetic.

• Parallel Form

-- Parallel connection of 1st order and 2nd order factors

$$H(z) = \sum_{k=0}^{N_p} C_k z^{-k} + \sum_{k=1}^{N_s} \frac{e_{ok} + e_{1k} z^{-1}}{1 - a_{1k} z^{-1} - a_{2k} z^{-2}}$$



Figure 6.20 Parallel-form structure for sixth-order system (M = N = 6) with the real and complex poles grouped in pairs.

• Feedback in IIR Systems

-- Basic formula of a feedback system (negative feedback)

$$H(z) = \frac{F(z)}{1 + F(z)B(z)}$$

-- If a system has poles, a corresponding block diagram or signal flow graph will have feedback loops.

(BUT neither poles in the system function nor loops in the network are sufficient for the impulse response to be infinitely long.)

-- A delay element is necessary in the feedback loop; otherwise, it is *noncomputable*. (The structure should be modified to eliminate the noncompuable loops.)



- Transpose Forms
 - -- *Transposition* of a flow graph is reversing the *directions* of *all* branches in the network while keeping the branch transmittances (as they were) and reversing the roles of the input and output (so that source nodes become sink nodes and vice versa).
 - -- Flow Graph Reversal Theorem

For single-input, single-output systems, the transposed flow graph has the same system function as the original graph if the input nodes and output nodes are interchanged.





Figure 6.27 Direct form II structure for Example 6.8.

Figure 6.28 Transposed direct form II structure for Example 6.8.



• Direct Form

-- Transversal filter or tapped delay line

$$y[n] = \sum_{k=0}^{M} b_k x[n-k]$$
 -- convolution



Figure 6.32 Transposition of the network of Figure 6.31.

Cascade Form

-- Serial connection of 1st order and 2nd order factors

$$H(z) = \prod_{k=1}^{M_s} (b_{ok} + b_{1k} z^{-1} + b_{2k} z^{-2})$$

Remark: Each factor is a Direct Form.



Figure 6.33 Cascade-form realization of an FIR system.

• Linear Phase FIR Filters

■ Take the advantage of the symmetry property of the impulse response

$$h[M - n] = h[n]$$

$$h[M - n] = -h[n]$$

$$y[n] = \sum_{k=0}^{M} h[k]x[n - k]$$

Type I or III: *M* even (order odd)

$$y[n] = \sum_{k=0}^{M/2-1} h[k]x[n-k] + h\left[\frac{M}{2}\right]x\left[n-\frac{M}{2}\right] + \sum_{k=\frac{M}{2}+1}^{M} h[k]x[n-k]$$
$$= \sum_{k=0}^{\frac{M}{2}-1} h[k](x[n-k] \pm x[n-M=k]) + k\left[\frac{M}{2}\right]x\left[n-\frac{M}{2}\right]$$

Type II or IV: *M* odd (order even)

$$y[n] = \sum_{k=0}^{\frac{M-1}{2}} h[k](x[n-k] \pm x[n-M+k])$$



Linear-phase FIR filters can also be implemented as a cascade of 1st-order, 2nd-order, and 4th-order real-coefficient systems. (The 4th-order system is formed by grouping the conjugate and the conjugate reciprocal zeros together.)



♦ Finite-precision Numerical Effects

- Due to finite-precision (finite-word length) of computational and/or storage devices.
 - -- Parameter quanitization
 - -- Round-off error
 - -- Limit cycle (IIR) ← zero input!
- Number Representation -- Two's complement number representation

$$\widehat{x} = X_m \underbrace{\left(-b_0 + \sum_{i=1}^{B} b_i 2^{-i}\right)}_{\widehat{x}_B = b_0 b_1 b_2 \dots b_B} \\ \left(-1 \le \widehat{x}_B < 1\right)$$
$$\therefore \quad -X_m \le \widehat{x} < X_m$$
$$\Delta = X \cdot 2^{-B}$$

 $\hat{x} = Q_B[x]$: quantized value of x

 \hat{x}_B : normalized quantized value of *x*; normalized value of \hat{x}

 Δ : quantization stepsize

 b_0 : sign bit; b_0 =0, if x is non-negative; b_0 =1, if x is negative.

- Quantization error $e = Q_B[x] x$
 - (1) Overflow: if $x > X_m$. This can be a serious problem if, for example, 0111 \rightarrow 1000,

and we don't check it first. (This is *natural overflow*.) We first clip the input. It becomes *saturation*.

(2) -- Rounding: nearest integer
$$-\Delta/2 < e \leq \Delta/2$$

-- Truncation: smaller integer $-\Delta < e \le 0$



• Quantization in implementing systems

$$H(z) = \frac{1}{1 - az^{-1}}$$



Figure 6.39 Implementation of discrete-time filtering of an analog signal. (a) Ideal system. (b) Nonlinear model. (c) Linearized model.

(c)

♦ Effects of Coefficient Quantization

• Coefficient Quantization in IIR Systems

- -- depends on the filter structure
- Direct form

$$H(z) = \frac{\sum_{k=0}^{M} b_{k} z^{-k}}{\underbrace{1 - \sum_{k=1}^{N} a_{k} z^{-k}}_{A(z)}} \to \widehat{H}(z) = \frac{\sum_{k=0}^{M} \widehat{b}_{k} z^{-k}}{1 - \sum_{k=1}^{N} \widehat{a}_{k} z^{-k}}$$

Note: $\hat{a}_k = a_k + \Delta a_k$; $\hat{b}_k = b_k + \Delta b_k$

Effect on pole locations

 $(\rightarrow$ affect frequency response and stability)

Compare
$$\begin{cases} A(z) = 1 - \sum_{k=1}^{N} a_k z^{-k} = \prod_{j=1}^{N} (1 - z_j z^{-1}) \\ \widehat{A}(z) = 1 - \sum_{k=1}^{N} \overline{a}_k z^{-k} = \prod_{j=1}^{N} (1 - \overline{z}_j z^{-1}) \end{cases}$$

The change of pole location: $\hat{z}_j = z_j + \Delta z_j$, j = 1,..., N

$$\Delta z_k \quad \text{is affected by all } \{\Delta a_k\}.$$
$$\Delta z_i \approx \sum_{k=1}^N \left(\frac{\partial z_i}{\partial a_k}\right) \Delta a_k, \quad i = 1, 2, ..., N$$

Remark: This formula is approximately true when Δa_k and Δz_k are small.

Note that if $\frac{\partial z_i}{\partial a_k}$ is large, then a small Δa_k leads to a large Δz_k . If so, this is a *sen*-

sitive system. (Undesirable)

One step further,

$$\frac{\partial z_i}{\partial a_k} = \frac{z_i^{N-k}}{\prod_{j=1, j \neq i}^N (z_i - z_j)} \cdot \begin{pmatrix} \left(\frac{\partial A(z)}{\partial z_i}\right)_{z=z_i} \frac{\partial z_i}{\partial a_k} = \frac{\partial A(z)}{\partial a_k} \Big|_{z=z_i} \end{pmatrix} \prod_{i \neq j} \left(1 - z_i^{-1} \cdot z_j\right) = z_i^{-k}$$

That is, if $(z_i - z_j)$ is small, then $\frac{\partial z_i}{\partial a_k}$ is large; for example, narrow bandwidth

lowpass and bandpass filters which have clustered poles. *Remark:* The preceding analysis can be applied to zeros.

Parallel and cascade forms

-- consists of 1st-order and 2nd-order sections.

Errors in a particular pole pairs (section) are independent of the other poles (sections).

This is also true for zeros in cascade form. \rightarrow In general, both the *cascade form* and the *parallel form* are less sensitive to coefficient quantization (because zeros are often widely distributed the unit circle).

Example: Bandpass IIR elliptic filter

$0.99 \le \left H(e^{jw}) \right \le 1.01$	$0.3\pi \le \omega \le 0.4\pi$	
$ H(e^{jw}) \le 0.01$ (-40dB)	$\omega \leq 0.29\pi$	
$ H(e^{jw}) \le 0.01 (-40 \text{dB})$	$0.41\pi \le \omega \le \pi$	

TABLE 6.1 UNDUANTIZED CASCADE FORM COEFFICIENTS FOR A 12TH-ORDER ELLIPTIC FILTER

k	a , , ,	424	bot	b	b 24
1	0.738409	-0.850835	0.135843	0.026265	0.135843
2	0.960374	-0.860000	0.278901	-0.444500	0.278901
3	0.629449	-0.931460	0.535773	-0.249249	0.535773
4	1.116458	-0.940429	0.697447	- 0.891543	0.697447
5	0.605182	-0.983693	0.773093	-0.425920	0.773093
6	1.173078	-0.986166	0.917937	- 1.122226	0.917937

 TABLE 6.2
 SIXTEEN-BIT QUANTIZED CASCADE-FORM COEFFICIENTS FOR A

 12TH-ORDER ELLIPTIC FILTER

k	a_{1k}	a_{2k}	b_{0k}	b_{1k}	b_{2k}
1	24196×2^{-15}	-27880×2^{-15}	17805×2^{-17}	3443×2^{-17}	17805×2^{-17}
2	31470×2^{-15}	-28180×2^{-15}	18278×2^{-16}	-29131×2^{-16}	18278×2^{-16}
3	20626×2^{-15}	-30522×2^{-15}	17556×2^{-15}	-8167×2^{-15}	17556×2^{-15}
4	18292×2^{-14}	-30816×2^{-15}	22854×2^{-15}	-29214×2^{-15}	22854×2^{-15}
5	19831×2^{-15}	-32234×2^{-15}	25333×2^{-15}	-13957×2^{-15}	25333×2^{-15}
6	19220×2^{-14}	-32315×2^{-15}	15039×2^{-14}	-18387×2^{-14}	15039×2^{-14}





Figure 647 (continued) (d) Passband for parallel structure with 16-bit coefficients. (c) Log magnitude for direct form with 16-bit coefficients. (f) Passband for normalized lattice with 16-bit coefficients.

• Second-order Section (1) Direct form

Poles: $(re^{j\theta}, re^{-j\theta})$

$$\frac{1}{\left(1 - re^{j\theta}z^{-1}\right)\left(1 - re^{-j\theta}z^{-1}\right)} = \frac{1}{1 - 2r\cos\theta z^{-1} + r^2 z^{-2}}$$



Figure 6.41 Direct-form implementation of a complex-conjugate pole pair.



(2) Coupled form

Poles: $(re^{j\theta}, re^{-j\theta})$ $\begin{cases}
Y_1 = X + r\cos\theta z^{-1}Y_1 - r\sin\theta z^{-1}Y \\
Y = r\sin\theta z^{-1}Y_1 + r\cos\theta z^{-1}Y \\
\Rightarrow Y_1 = (z - r\sin\theta z^{-1}Y)/1 - r\cos\theta z^{-1} \\
\frac{Y}{X} = \frac{(r\sin\theta)z^{-1}}{1 - 2r\cos\theta z^{-1} + r^2 z^{-2}}
\end{cases}$



Figure 6.43 Coupled-form implementation of a complex-conjugate pole pair.



 \rightarrow The pole location distribution is even.

← The price: The number of multiplications is doubled!

• Coefficient Quantization in FIR Systems

Direct form

$$H(z) = \sum_{n=0}^{M} h[n] z^{-n} \rightarrow \widehat{H}(z) = \sum \widehat{h}[n] z^{-n}$$

$$= H(z) + \underbrace{\Delta H(z)}_{\sum \Delta h[n] z^{-n}}$$

$$\Delta H(z) = \sum_{n=0}^{M} \Delta h[n] z^{-n}$$

Effect on the zero locations

The sensitivity function of this form is similar to that of the direct form I IIR filter. That is, if the zeros are tightly clustered, their locations will then be highly sensitive to quantization errors. However, for most linear phase FIR systems, the zeros are more or less uniformly spread in the z-plane.

<u>Effect on $H(e^{j\omega})$ </u>

After scaling, each h[n] is represented by (B+1) bits 2's complement number; i.e.,

$$-2^{-(B+1)} < \Delta h[n] \le 2^{-(B+1)}$$

$$\Delta H\left(e^{j\omega}\right) = \sum_{n=0}^{M} \Delta h[n] e^{-j\omega n}$$

$$\left|\Delta H\left(e^{j\omega}\right)\right| = \left|\sum_{n=0}^{M} \Delta h[n] e^{-j\omega n}\right| \leq \sum_{n=0}^{M} \left|\Delta h[n]\right| e^{-j\omega n} \left|$$

$$\leq (M+1) 2^{-(B+1)}$$
ward card

Effect on linear phase

Not affect the linear phase property as long as $\hat{h}[n] = \hat{h}[M - n]$.

Example: Linear Phase Lowpass Filter

$0.99 \le \left H(e^{jw}) \right $	≤1.01	$0\!\le\!\omega\!\le\!0.4\pi$
$\left H(e^{jw})\right \leq 0.00$	01 (-60dB)	$0.6\pi \le \omega \le \pi$

TABLE 6.3 UNQUANTIZED AND QUANTIZED COEFFICIENTS FOR AN OPTIMUM FIR LOWPASS FILTER (M = 27)

Coefficient	Unquantized	16 bits	14 bits	13 bits	8 bits
h[0] = h[27]	1.359657×10^{-3}	45×2^{-15}	11×2^{-13}	6×2^{-12}	0×2^{-7}
h[1] = h[26]	-1.616993×10^{-3}	-53×2^{-15}	-13×2^{-13}	-7×2^{-12}	0×2^{-7}
h[2] = h[25]	-7.738032×10^{-3}	-254×2^{-15}	-63×2^{-13}	-32×2^{-12}	-1×2^{-7}
h[3] = h[24]	-2.686841×10^{-3}	-88×2^{-15}	-22×2^{-13}	-11×2^{-12}	0×2^{-7}
h[4] = h[23]	1.255246×10^{-2}	411×2^{-15}	103×2^{-13}	51×2^{-12}	2×2^{-7}
h[5] = h[22]	6.591530×10^{-3}	216×2^{-15}	54×2^{-13}	27×2^{-12}	1×2^{-7}
h[6] = h[21]	-2.217952×10^{-2}	-727×2^{-15}	-182×2^{-13}	-91×2^{-12}	-3×2^{-7}
h[7] = h[20]	-1.524663×10^{-2}	-500×2^{-15}	-125×2^{-13}	-62×2^{-12}	-2×2^{-7}
h[8] = h[19]	3.720668×10^{-2}	1219×2^{-15}	305×2^{-13}	152×2^{-12}	5×2^{-7}
h[9] = h[18]	3.233332×10^{-2}	1059×2^{-15}	265×2^{-13}	132×2^{-12}	4×2^{-7}
h[10] = h[17]	-6.537057×10^{-2}	-2142×2^{-15}	-536×2^{-13}	-268×2^{-12}	-8×2^{-7}
h[11] = h[16]	-7.528754×10^{-2}	-2467×2^{-15}	-617×2^{-13}	-308×2^{-12}	-10×2^{-7}
h[12] = h[15]	1.560970×10^{-1}	5115×2^{-15}	1279×2^{-13}	639×2^{-12}	20×2^{-7}
h[13] = h[14]	4.394094×10^{-1}	14399×2^{-15}	3600×2^{-13}	1800×2^{-12}	56×2^{-7}



Cascade form

-- less sensitive because it isolate the quantization errors from the other sections.

- -- To preserve linear phase each section is linear phase.
 - (a) Conjugate 2nd-order sections for conjugate zero pairs on the unit circle. $(1 + az^{-1} + z^{-2})$
 - (b) Real zero 2nd-order sections for a real zero inside the unit circle and its reciprocal (outside the unit circle).
 - (c) Zeros at ± 1 .
 - (d) 4th-order sections for conjugate zero pairs inside the unit circle and their associated reciprocals (outside the unit circle).



Figure 6.48 Subnetwork to implement fourth-order factors in a linear-phase FIR system such that linearity of the phase is maintained independently of parameter quantization.